

Physics Design of Stellarators

A. Bader¹, B.J. Faber¹, M. Drevlak², C.C. Hegna¹,
H. Frerichs¹, J.C. Schmitt³

1) University of Wisconsin-Madison

2) IPP-Greifswald 3) Auburn University

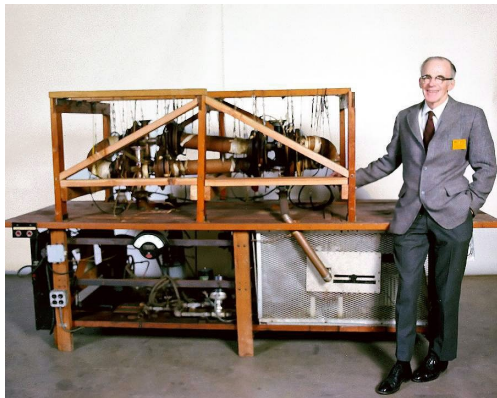
9th International Workshop on Stochasticity in Fusion Plasmas
3D Physics in Tokamaks and Stellarators
Bad Honnef, Germany Apr 8, 2019



WISCONSIN
UNIVERSITY OF WISCONSIN-MADISON

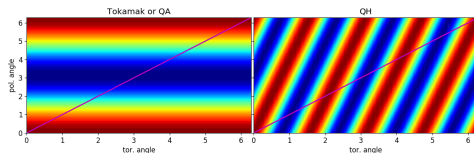
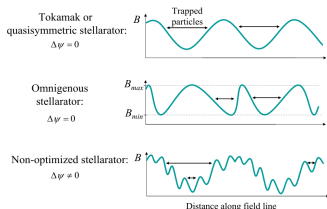
- 1 How do you design an optimized stellarator?
- 2 Designing a stellarator: Optimization in practice
 - Neo-classical optimization
 - Energetic particle optimization - testing a metric
 - Optimizing for turbulence - designing a metric
 - Coils - Closing the loop

Stellarators are one of the earliest fusion concepts



- Lyman Spitzer invented the stellarator concept in 1953
- Early stellarators suffered from large neo-classical losses
 - Trapped particles precess
 - Axisymmetry: precession is toroidal
 - Non-axisymmetry: precession can have a radial component

Good confinement is attainable in non-axisymmetric systems



M. Landreman APS invited talk
2012

- If all maxima and minima of $|\mathbf{B}|$ align when following a field line, bounce averaged radial drift is zero
- If $|\mathbf{B}|$ along field is close to sinusoidal, the configuration is quasi-symmetric (or symmetric)

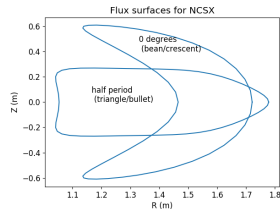
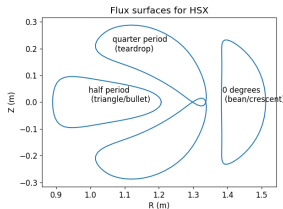
Equilibria are defined by boundaries, $p(\psi)$, and $J(\psi)$

$$R(\theta, \zeta) = \sum_{m,n} R_{c,mn} \cos(m\theta - n\zeta) + R_{s,mn} \sin(m\theta - n\zeta)$$

$$Z(\theta, \zeta) = \sum_{m,n} Z_{c,mn} \cos(m\theta - n\zeta) + Z_{s,mn} \sin(m\theta - n\zeta)$$



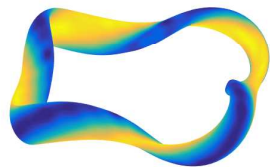
- Boundaries given in Fourier series
- Optimized stellarators typically go from bean-like cross-sections to triangle-like cross-sections



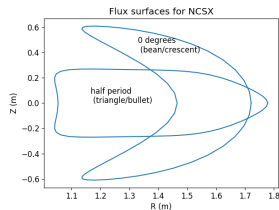
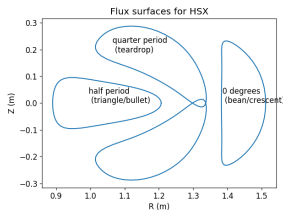
Equilibria are defined by boundaries, $p(\psi)$, and $J(\psi)$

$$R(\theta, \zeta) = \sum_{m,n} R_{c,mn} \cos(m\theta - n\zeta) + \cancel{R_{s,mn} \sin(m\theta - n\zeta)} \rightarrow 0$$

$$Z(\theta, \zeta) = \sum_{m,n} \cancel{Z_{c,mn} \cos(m\theta - n\zeta)} \rightarrow 0 + Z_{s,mn} \sin(m\theta - n\zeta)$$

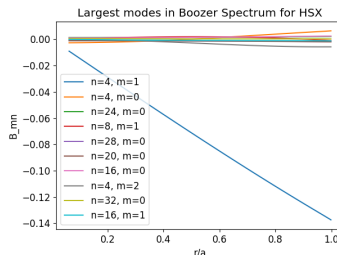
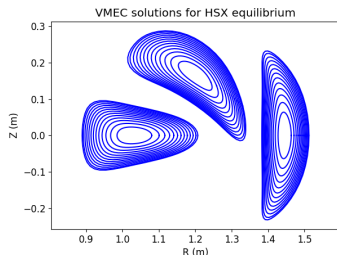


- Boundaries given in Fourier series
- Optimized stellarators typically go from bean-like cross-sections to triangle-like cross-sections



3D geometry allows optimization in novel ways

- Boundary $\rightarrow$ Eq. solution $\rightarrow$ Coord. transformations $\rightarrow$ evaluation



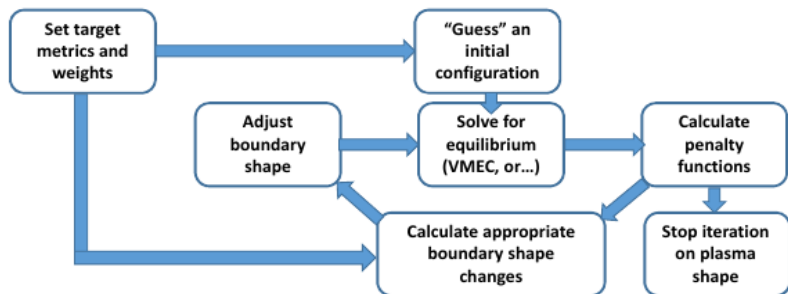
Standard metrics

- Rotational transform, $\iota(\psi)$
- Quasisymmetry metric, $Q(\psi)$
- Neo-classical transport, $\epsilon(\psi)$, $\chi \sim \epsilon(\psi)$
- Bootstrap current, $J_{bs}(\psi)$
- Magnetic well, aspect ratio, volume

New metrics

- Energetic particle confinement
- Turbulent transport
- Coil properties

Optimizing the boundary with modern computation



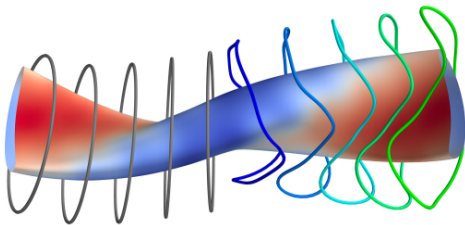
- Optimization codes include `STELLOPT` and `ROSE`
- Usually optimization schemes are modified gradient descents

Optimizer evaluates performance based on user selected penalty functions, p_i , targets t_i and weights w_i

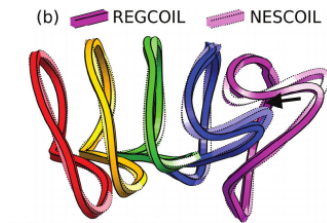
$$F(\{R_{mn}, Z_{mn}\}) = \sum_i w_i [p_i(\{R_{mn}, Z_{mn}\}) - t_i]^2$$

Producing the configuration with coils

Typically coil design is done after an equilibrium is found
This requires iterations between the plasma equilibrium and a coil code to find an adequate solution for both.



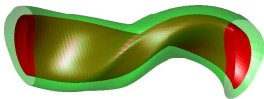
C. Zhu NF **58** (2017)



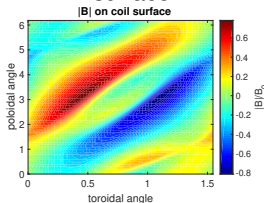
M. Landreman NF **57** (2017)

Standard approach - solve for current potential on external surface

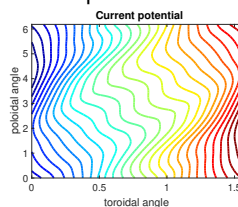
Start with target and coil surfaces



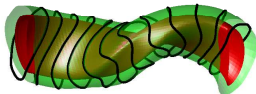
Calculate $|B|$ on coil surface



Integrate to get current potential



Map current potential back onto coil surface



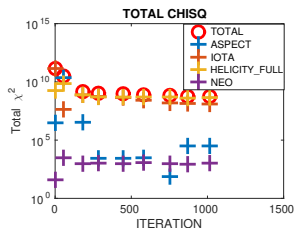
- This approach was used to generate coils for W7-X and HSX
- Modern computational power allows for improvements

1 How do you design an optimized stellarator?

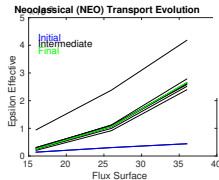
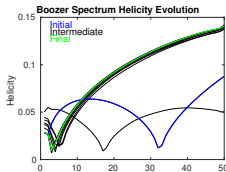
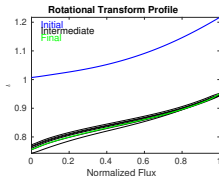
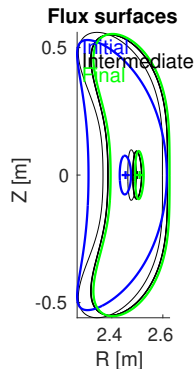
2 Designing a stellarator: Optimization in practice

- Neo-classical optimization
- Energetic particle optimization - testing a metric
- Optimizing for turbulence - designing a metric
- Coils - Closing the loop

Example - optimize to alter rotational transform profile



- Major focus is on ι profile at fixed aspect ratio
- However, try to keep good QS and neoclassical transport

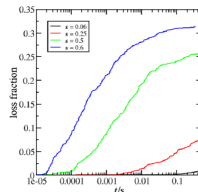


Energetic particle confinement is a key issue in stellarators

- Prompt alpha particle losses can cause significant damage to first wall
- Example - ARIES reactor study found 5% alpha energy losses
- Alpha losses alone exceeded wall heat flux limits at several places
- Evaluation of energetic particle confinement is usually done with Monte-Carlo
 - Computationally expensive
 - Obscures physics mechanisms

Possible metrics for energetic particle optimization

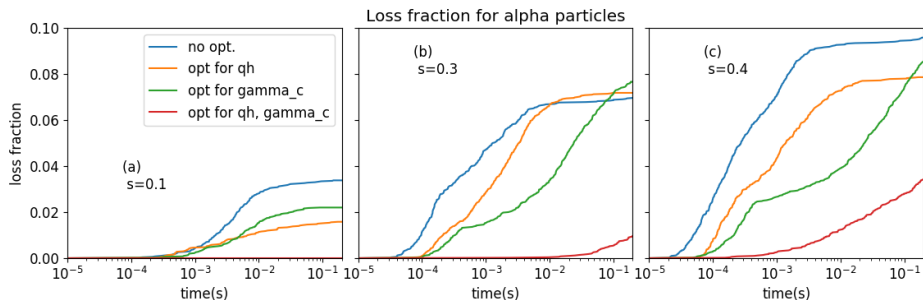
- ϵ_{eff} : standard optimization for neo-classical transport
 - Focuses on deeply trapped particles
 - Less effect on particles near trapped-passing boundary
- Quasi-symmetry
 - Perfect quasi-symmetry has no particle losses
 - Perfect quasi-symmetry is not actually attainable
- $\gamma_c = \arctan(v_r/v_\theta)$
 - Seeks to reduce ratio of radial to poloidal drift by aligning J contours
 - Successful at optimizing QH



Henneberg NF 2019

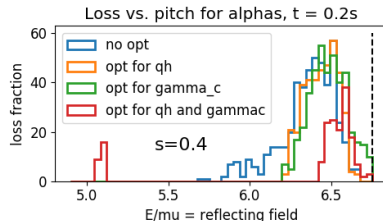
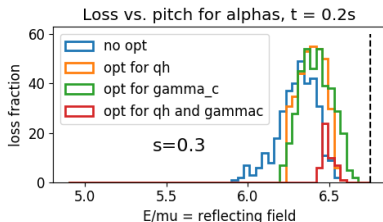
Nemov PoP 1999, Spong PoP 1998, Nemov PoP 2008

Best performance when optimization for Γ_c and quasisymmetry



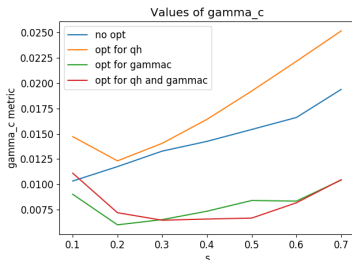
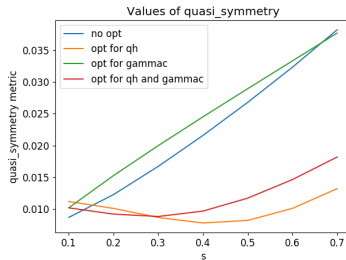
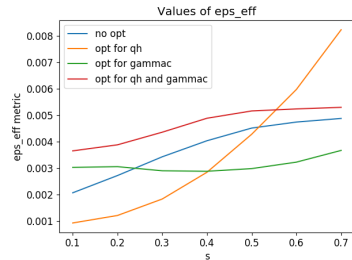
- All configurations scaled to 450 m^3 and $B_0 = 5.6 \text{ T}$
- $\Gamma_c \sim \sum_{E/\mu} \sum_{\text{wells}} \int_b \arctan^2(v_r/v_\theta) \tau_b$
- Prompt losses entirely eliminated in best performing case (red); all losses eliminated inside $s = 0.1$

Particle losses at trapped passing boundary are suppressed



- Most problematic region is near the trapped passing boundary
- The best confinement case (red) sacrifices confinement of deeply trapped particles to better confine particles near the trapped passing boundary

ϵ_{eff} is not the correct metric for energetic particles

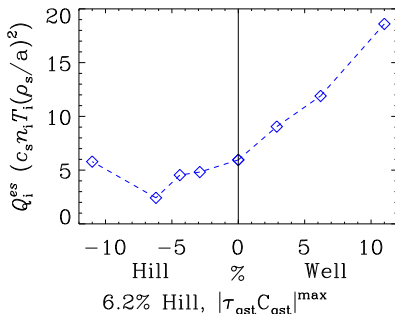
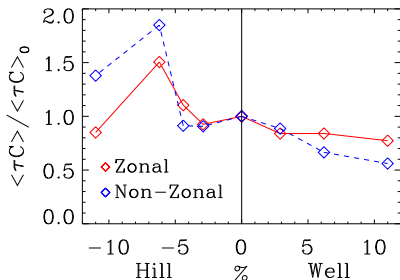


- Improvement of alpha confinement in **red** configuration despite worse ϵ_{eff} across most of the radius

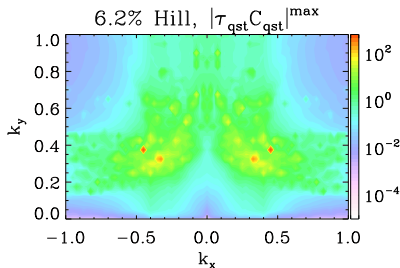
Using energy transfer as a turbulent transport metric

- Stable modes can provide an energy sink at instability scales
- Stable modes couple to linear instability through 3-wave nonlinearity.
 - Heat flux is inversely proportional to a correlation time, τ
 - $Q \propto \sum_{i,j,k} \frac{1}{k_{\perp}^2} \frac{\gamma_k}{\tau}$, $\tau_{ijk} = 1/i(\omega_i^* - \omega_j - \omega_k)$
 - Key idea: maximize correlation lifetimes between unstable and stable modes
- Geometry and plasma profiles determine the ω values

Turbulence metric reproduces non-linear gyrokinetics

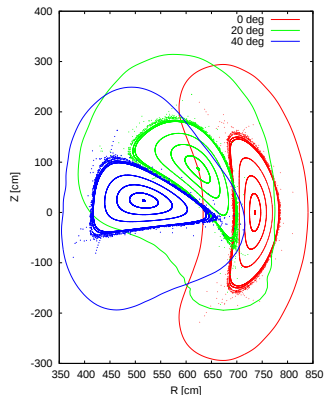
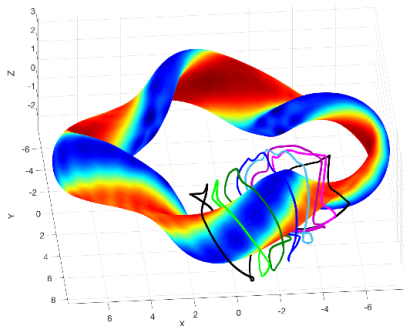


- Metric anti-correlated with gyrokinetic Q as predicted
- Resonances of $1/\tau$ at specific k_x, k_y cause improved performance



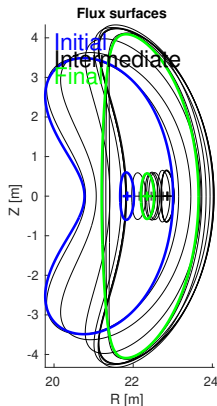
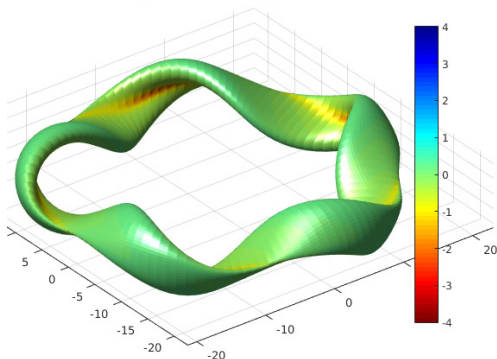
Incorporating coil codes directly into equilibrium optimization

- Increases search space considerably
- May require better optimization algorithms



Designing metrics for ease of coil design

- Sensitive locations for coils correspond to areas of high second principal curvature of the boundary
- These areas can be directly targeted in optimization codes

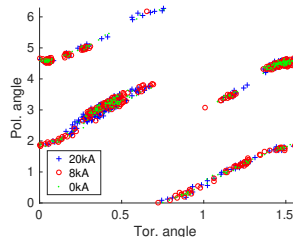
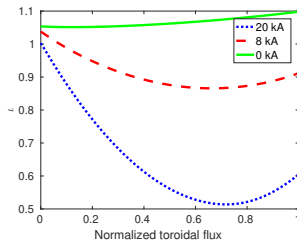
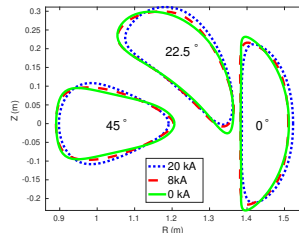
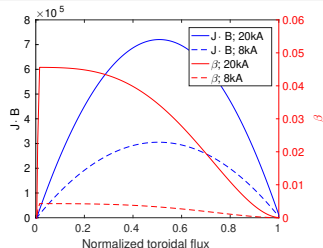


We are ready to design the next generation of optimized stellarator

- Stellarator optimization has been successfully implemented on HSX and W7-X
 - Optimizer codes manipulate plasma boundaries and evaluate the resulting equilibria
 - Separate codes determine coil shapes
- Using 3D nature of stellarators we can optimize configurations in completely new ways
 - New metrics for energetic particle confinement and turbulent transport are being tested and developed
 - Coil metrics or coil design itself can be included in the physics optimization
 - Development of better optimization algorithms and boundary representations is ongoing

Extra slides

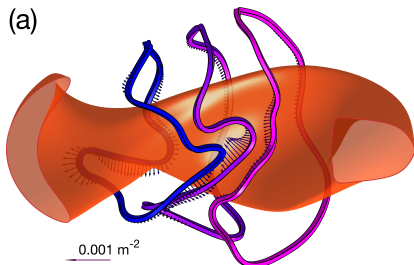
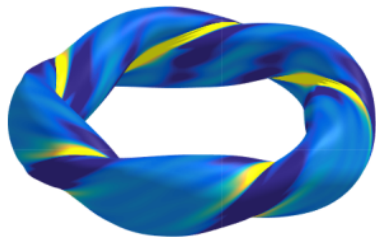
Non-resonant divertors resilient to plasma evolution



No difference is noticeable with shape changes from plasma!

A. Bader PoP **24** (2017) 032506

Coil sensitivity and divertor locations



- Shape gradient calculations indicate regions of high sensitivity
- Sensitive regions are far away from desirable divertor locations

E.J. Paul NF **58** (2018) 076015; M. Landreman NF **58** (2018) 076023